General Disclaimer

One or more of the Following Statements may affect this Document

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some
 of the material. However, it is the best reproduction available from the original
 submission.

Produced by the NASA Center for Aerospace Information (CASI)

REQUIREMENTS AND CAPABILITIES FOR PLANETARY MISSIONS: Venus Orbiter Imaging Radar 1983

Jet Propulsion Laboratory California Institute of Technology Pasadena, California 91103

(NASA-CR-148734) REQUIREMENTS AND CAPABILITIES FOR PLANETARY MISSIONS. VENUS ORBITER IMAGING RADAR 1983, VOLUME 3 (Jet Propulsion Lab.) 9 p HC \$3.50 CSCL 22B

N76-30280

G3/18 Unclas 50448



August 1976

1. Report No. 43-27, Vol. 3	2. Government Accession No.	3. Recipient's Catalog No.		
4. Title and Subtitle REQUIREMENTS AND CAPABILITIES FOR PLANETARY		5. Report Date August 1976		
MISSIONS: VENUS ORBITER		6. Performing Organization Code		
7. Author(s) D. H. Kindt, G. G	8. Performing Organization Report No.			
9. Performing Organization Name and JET PROPULSION LABO		10. Work Unit No.		
California Institut 4800 Oak Grove Driv	e of Technology	11. Contract or Grant No. NAS 7-100		
Pasadena, Californi		13. Type of Report and Period Covered Special Publication		
12. Sponsoring Agency Name and Add	ress	Special Publication		
NATIONAL AERONAUTICS AND S Washington, D.C. 20546	PACE ADMINISTRATION	14. Sponsoring Agency Code		
15. Supplementary Notes				
1/				
under consideration. The at about the 200-m resolution cal studies. Science in of the planet, study the mass distribution. A planet.	e objective of the mission ution level, with continuivestigations will determine surface/atmosphere interpolations vehicle is based considered include a Lun	Alliptical orbits are also in is imagery of the planet, lous altimetry and topographine surface characteristics factions, and determine Venus on a Mariner Jupiter/Saturn far Polar Orbiter derivative		
17. Key Words (Selected by Author(s))	18. Distributi	Unclassified Unlimited		
Spacecraft Design, Testi: Performance Lunar and Planetary Explo (Advanced)				
19. Security Classif. (of this report)	20. Security Classif. (of this	page) 21. No. of Pages 22. Price		
Unclassified	Unclassified	6		

REQUIREMENTS AND CAPABILITIES FOR PLANETARY MISSIONS: Venus Orbiter Imaging Radar 1983

D. H. Kindt G. G. Ball T. H. Bird

Jet Propulsion Laboratory California Institute of Technology Pasadena, California 91103

August 1976

Foreword

This volume represents one of a series of requirements and capabilities for planetary missions assembled from recent study activities at JPL. The purpose of this series of documents is to provide a summary of these studies which may be readily used in subsequent efforts. Emphasis is upon requirements and associated capabilities of the spacecraft and mission design at developed in the study. No particular priority of individual missions should be assumed from the sequence of these reports.

The other published volumes in this series are SP 43-27, Vol. 1, Mariner Encke Ballistic Flyby 1980, November 1975, and SP 43-27, Vol. 2, Mars Polar Orbiter/Penetrator 1981, March 1976. These volumes were prepared by the Mission Engineering Section of the Project Engineering Division.

Venus Orbiter Imaging Radar

Launch Date: April-June 1983

Encounter Date: October-November

1983

Injection Mass: 4335 kg
Net Mass in Orbit: 735 kg
Instrument Mass (radars only): 57 kg

Launch Vehicle: Shuttle/IUS

Objectives:

Imagery of the whole planet, at about the 200-m resolution level, with continuous altimetry for determination of surface changes and features, and topographical studies. Some high-resolution imagery at about 50 m could be available.

Typical Science Investigations:

Synthetic aperture radar Additional science investigations under study

Mission Description:

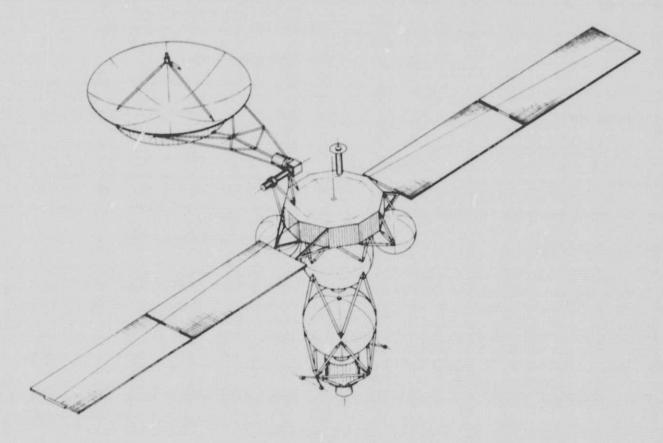
Two spacecraft are inserted into a 97-min, 500-km circular polar orbit. Elliptical orbits are under consideration, the tradeoff being propulsion system requirements vs. radar system complexity and performance. Imaging occurs on specific defined orbits, while other activities such as nonradar science, altimetry, and telecommunications take place on nonimaging orbits. The circular orbit allows complete planet mapping within 120 days. A plausible vehicle for a Venus Orbiter Imaging Radar (VOIR) mission is based on a Mariner Jupiter/Saturn (MJS) derivative, with some design inheritance from Viking and other Mariner spacecraft. The VOIR spacecraft has solar panels.

Other spacecraft concepts being considered include a Lunar Polar Orbiter derivative with a Seasat-type antenna and a multiantenna Pioneer Venus Orbiter derivative with some despun parts.

I. Science

A. Rationale

Imaging and mapping of the surface of Venus significantly beyond the capabilities of Earth-based observations would be a major step in the exploration of the terrestrial



planets. The VOIR mission represents a practical, realizable means of meeting this need in the 1980s using side-looking radar.

B. Objectives

Science objectives appropriate to this mission are:

- To determine surface characteristics such as texture, crustal structure, topography, and morphology.
- (2) To study the surface/atmosphere interactions of Venus.
- (3) To examine meteorite impact effects on the surface and phenomena such as cratering, brecciation melting, erosion, and regolith formation.
- (4) To determine the mass distribution of Venus.

C. Typical Experiments

The synthetic aperture radar (SAR) is the only proposed science instrument carried on the VOIR spacecraft in this study. This radar could be similar in concept to the one to be flown on Seasat-A in 1978. The SAR would operate at L-band frequencies (1 to 2 GHz), at an altitude from the surface of 500 km, and would be used for imaging as well as altimetry.

Other scientific instruments could be flown and are under investigation.

II. Mission Description

A. Launch and Arrival

The VOIR mission involves two spacecraft being inserted into a 500-km circular polar orbit around Venus. Launch opportunities open in April 1983 for arrival in late October and early November 1983. For this period, C_3 s of less than 12.0 km²/s² are required over a 70-day injection period beginning in April.

The spacecraft is launched using the Shuttle/IUS, with an expected injection capability from 5500 to 6200 kg over a 6.0 to $12.0~\rm km^2/s^2$ C_3 range.

Launching the two spacecraft with a single set of launch equipment may be considered even with coincident launch and injection periods. A 22-day launch period is adequate if dual sets of launch equipment are available; 52 days are required if a single set of launch equipment is used.

The cruise period to Venus after injection by the Shuttle/IUS takes about 4 months. The arrival speed of the spacecraft at Venus ranges from 2.9 to 4.1 km/s, depending upon when the launch occurs in the April 1983 launch period.

B. Venus Orbit

The nominal orbit selected is a 500-km-altitude polar circular orbit, which has the following advantages:

- The radar doppler shift requirements are minimized by the circular orbit.
- (2) No undue navigation and atmospheric uncertainties are encountered at the low orbital altitude; hence the radar design requirements are eased. (A more extensive analysis would be required to justify any significant further reduction in altitude.)
- (3) The circular polar orbit allows complete planet mapping within 120 days.

An alternate circular polar orbit could be achieved by increasing the altitude to 1000 km. More radar power and a somewhat longer time would be needed for Venus mapping. However, this type of orbit would also provide some relief of the orbit determination problems associated with the lower circular orbit. A 500×1000 km elliptical orbit could be utilized but would have a serious impact on radar design complexity and data analysis.

C. Data Management

The data collection philosophy for this mission assumes that the radar mapping objectives will be accomplished during the first half of a Venusian rotation period. The revolution-to-revolution shift of the spacecraft's ground trace is less than the typical radar swath width, permitting complete mapping of the surface in one half of a Venusian rotation period. Optimization of system operations could be achieved by having the radar operate continuously over this period. After the mapping requirements were satisfied, the remaining orbits could be used for collecting other science data and data transmission.

III. General Spacecraft Characteristics

The baseline VOIR spacecraft that has been studied is a three-axis stabilized design based on existing MJS technology (Figs. 1 and 2). This spacecraft is solar powered and has a relatively large propulsion system, with radar added as the main science experiment.

The spacecraft structure consists of an MJS'77 ten-sided bus. It supports all appendages and provides a structural

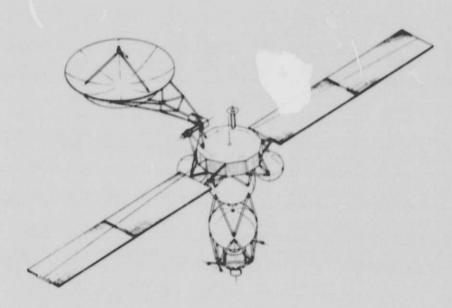


Fig. 1. VOIR spacecraft (Earth-storable propellants)

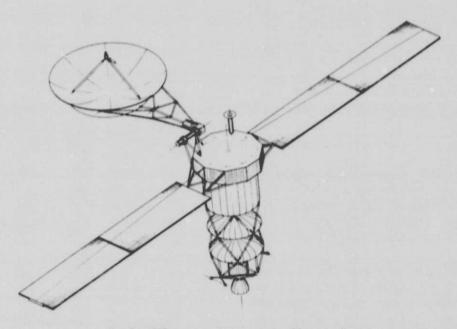


Fig. 2. VOIR spacecraft (space-storable propellants)

foundation for the subsystems as well as a propulsion support structure.

Attached to the bus via outriggers are deployable solar panels. Based on a modified Viking design, they provide the power for the VOIR spacecraft. The two solar panels have a combined area of about 14.8 m². Additional power can be achieved by the use of two Ni-Cd batteries, along with other electrical power equipment. The total power needed by the spacecraft at launch is about 304 watts.

The propulsion system, located at the aft end of the bus, could consist of either of two major classes of propulsion systems. The first option utilizes advanced Earth-storable bipropellants and relies heavily on the Mariner Mars 1971 (MM'71) and Viking Orbiter 1975 (VO'75) propulsion technology. The major changes for the VOIR mission are the use of hydrazine (N_2H_4) rather than monoethylhydrazine (MMH) as the fuel, and the use of a modified 4.0-kN thrust Shuttle reaction control engine instead of the 1.3-kN MM'71 and VO'75 engines. The use of N_2H_4 provides

a 3% increase in specific impulse and increased thrust over conventional Earth-storable propellants. This allows insertion of the spacecraft into a 500-km circular orbit with one set of launch equipment and nominal IUS capability, but two burns of the insertion motor are require.

The second propulsion system option, space-storable propellants (fluorine/hydrazine), provides a significant improvement in specific impulse. Since the oxidizer in this case is a cryogenic, new spacecraft interface requirements result. The use of space-storable propellants permits capture of the baseline mission with a single burn, given nominal IUS capability. Multiple burns would allow the retro mass to be reduced significantly.

The telecommunications system is also based on MJS design. It consists of redundant X-band transmitters and S-band transmitters and receivers and the necessary supporting elements. The receivers obtain the uplink signal via the S-band low-gain antenna (LGA). The output of the X-band transmitters can be switched to the 3.1-m-diameter high-gain antenna (HGA) or to either of two X-band LGAs, a biconical (medium-gain) antenna, and a horn antenna. An L-band feed is added to the HGA for the radar.

The high-gain antenna requires three degrees of freedom for radar mapping of the surface of Venus and radar altimetric determination of surface features, as well as for high-bit-rate communications with Earth.

Radar mapping relies upon the ability of the antenna to be pointed continuously at a surface point 10 deg to the side of the subspacecraft point (surface intersection point of the radial line from the planet's center to the spacecraft). Radar altimetry requires that the antenna be aimed at the subspacecraft point on nonmapping orbits.

Antenna pointing requirements necessitate that high spacecraft attitude stability be maintained throughout the orbital portion of the VOIR mission. Antenna pointing is accomplished by three actuators which operate the three-degree-of-freedom antenna pointing mechanisms. The spacecraft is stabilized by an attitude control system based on the MJS'77 design. The Sun and Canopus are used as celestial references for attitude control.

Data handling and command functions are handled separately. Data compression techniques may be used separately or incorporated within the radar.

Data storage is provided by two (redundant) NASA standard 109-bit tape recorders, capable of recording and playback rates up to 5.88 Mb/s.

The VOIR requirements for data management are summarized in Tables 1 and 2.

Other subsystems used in the spacecraft, such as thermal control, cabling, and mechanical devices, are also based on MJS'77 design. Table 3 presents the VOIR spacecraft mass summary, including a breakdown of the two propulsion system options that could be used in this mission.

Table 1. Data requirements

Number of data streams	2
Science data rate	500 (uncoded)/250 kb/s (coded)
Engineering data rate	50/25 bits/s
Total number of engineering measurements	256
Engineering data frame size	128 measurements
Number of engineering formats	4
Engineering measurement length	8 bits
Science data format	Block of 2048 6-bit words
Bit error rate	< 5 × 10 ⁻⁶
Data storage requirement	1.2 × 10 ⁹ bits
Data record rates	0.5 and 5.8 Mb/s

Table 2. Control requirements

8
14
90
4 bits/s
42

Table 3. VOIR spacecraft mass summary

Subsystem		Mass kg		Remarks	
Structure		220.2	Includes solar panel structure and or	atriggers, and propulsion supp	port structure.
Radio frequency		40.0			
Modulation/demodulation		9.2			
Power		132.0			
Computer command		15.3			
light data		15.9			
Attitude and articulation control		118.9	Includes entire attitude-propulsion s hydrazine and helium (pressurant), actuators.		
Pyrotechnics		8.8	With VO'75-based propulsion actuation unit		
Cabling		41.8	Includes radar, solar panel, propulsion, and actuator cabling.		
Temperature control		22.7	Includes blanket for propulsion subsystem.		
Mechanical devices		21.0	Includes solar panel-related devices.		
Data storage		25.4			
S/X/L band antennas		6.9	Includes radar L-band feed for high-	gain antenna.	
S/X/L band antennas Radar		57.0	Includes radar L-band feed for high- Transmitter/receiver/power converte compressor 5.0 kg.		r assembly 22.0 kg, da
	Total		Transmitter/receiver/power converte		r assembly 22.0 kg, da
	Total	57.0	Transmitter/receiver/power converte compressor 5.0 kg.		r assembly 22.0 kg, da
Radar	Total	57.0	Transmitter/receiver/power converte compressor 5.0 kg.	er 30.0 kg, based on processor	
Radar		57.0	Transmitter/receiver/power converte compressor 5.0 kg.	Earth-storable	Space-storabl
Radar Propulsion inerts Total (dry spacecraft wi		57.0	Transmitter/receiver/power converte compressor 5.0 kg.	Earth-storable	Space-storabl
Radar Propulsion inerts		57.0	Transmitter/receiver/power converte compressor 5.0 kg.	Earth-storable 455.0 1190.1	Space-storabl 572.5 1307.6
Propulsion inerts Total (dry spacecraft wi Usable propellants		57.0	Transmitter/receiver/power converte compressor 5.0 kg.	Earth-storable 455.0 1190.1 3000.0	Space-storabl 572.5 1307.6 3027.0
Propulsion inerts Total (dry spacecraft wi Usable propellants (\(\Delta V\), m/s) Total (separated mass)	th APS fuel)	735.1	Transmitter/receiver/power converte compressor 5.0 kg.	Earth-storable 455.0 1190.1 3000.0 (3700)	572.5 1307.6 3027.0 (4350)

IV. Mission Options

Launch opportunities for VOIR are also available in November 1981 and December 1984. The former is somewhat inferior to the 1983 opportunity, while the latter is approximately equal to it. Both permit mission accomplishment with no increased performance difficulties.

A possible strategy to be considered is the addition of nonradar science instruments to the VOIR payload. These could include a mass spectrometer and a dayglow experiment, which would provide a greater understanding of the composition of the Venus atmosphere. A UV imaging instrument is another possibility. This equipment could take advantage of the spacecraft stability necessary for remote sensing by the radar.

Another possible option is the combination of a VOIR spacecraft with a high-attitude buoyant station. This station would float in the atmosphere of Venus and study atmospheric circulation and properties. The VOIR spacecraft could be the support and relay vehicle for the buoyant station.

Bibliography

- Adams, J.B., et al., "Strategy for Scientific Exploration of the Terrestrial Planets," Rev. Geophys., Vol. 7, pp.623-661, 1969.
- Asnin, S. K., "An Orbiter Radar Mapper of Venus in the 1980's," AAS Paper, AAS/AIAA Astrodynamics Conference, July 16, 1975.
- Friedman, L.D., and Rose, J.R., Final Report of Venus Orbiter Imaging Radar (VOIR) Study, 760-89, Jet Propulsion Laboratory, Pasadena, California, November 30, 1973 (JPL internal document).
- Kindt, D.H., Space Transportation System/Venus Orbital Imaging Radar, 760-143, Jet Propulsion Laboratory, Pasadena, California, April 30, 1976 (JPL internal document).
- Rose, J.R., and Friedman, L.D., "A Design for a Venus Orbital Imaging Radar Mission," AIAA Paper 74-222, 12th Aerospace Science Meeting, February 1, 1974.
- Saunders, R.S., Friedman, L.D., and Thompson, T.W., "Mission Planning for Remote Exploration of the Surface of Venus," AIAA Paper 73-580, AIAA/ ASMS/SAE Joint Space Mission Planning and Execution Meeting, July 10-12, 1973.
- Planetary Mission Summary; Venus Orbital Imaging Radar, SP 43-10, Vol. 12, Jet Propulsion Laboratory, Pasadena, California, August 1974 (JPL internal document).